



Norwegian  
Meteorological  
Institute

# AeroTab: look-up table code for aerosol optics and size-info (e.g. cloud drop activation)

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## Main subroutines of AeroTab.f, and their main purposes:

specbands	Define spectral bands, and sub-bands for Chandrasekhar averaging
constsize	Define constants and necessary aerosol parameters
openfiles	Open files for output (to use as input in CAM-Oslo)
modepar	Define log-normal size parameters and grids for use in the look-up tables
drydist	Define (calculate) dry modal background size distributions
condsub	Calculate diffusion coefficients
coagsub	Calculate coagulation coefficients
tabrefind	Read in and interpolate refractive indices for the used spectral bands
conteq -> smolar	Find process-modified size distributions of number and constituent mass by use of the Smolarkiewicz advection scheme
rhssub -> koehler -> mixsub -> smolar	Calulate hygroscopic growth by numerically solving the Köhler equation for all externally and internally mixed components, and using the Smolarkiewicz advection scheme
sizemie -> refind -> miev0 -> chandrap	Calculate gross optical properties (integrated over all or some sizes) Calculate refractive indices for internal mixtures (volume / Maxwell Garnett) Mie-calculations: qext, qsca, ggsc, sback Calculate chandrasekhar averaged optical properties for spectral bands consisting of several sub-bands
modetilp	Find log-normal fits to the process-modified number size distributions

## Setting up AeroTab to produce the needed lookup-tables, in AeroTab.f:

```
c Adjustable input parameters to the look-up table calculations:  
c Calculations for background aerosol modes 1 to 10 or mode 11 to 14  
c (itot=0), or total aerosol, mode 1-10 only (itot=1):  
c   itot=1  
c   Let iccn=0 for optics tables, iccn=1 for CCN (CAM-Oslo with DIAGNCDNC)  
c   --> ccnk*.out, or size distribution calculations (CAM4-Oslo and CAM5-Oslo  
c   with the prognostic CDNC scheme):  
c     iccn=0  
c   Lognormal mode fitting (itilp=1) or not (itilp=0) (requires iccn=1)  
c   --> logntilp*.out (and nkcomp.out for dry size distributions):  
c     itilp=1  
c   We only do the lognormal fitting only if iccn=1 (and for dry aerosols):  
c     if(iccn.eq.0) itilp=0  
c   Options for iccn=0 --> lwkcomp*.out or kcomp*.out, aerodryk*.out,  
c   aerocomk*.out, and nkcomp*.out (for size distributions for all RH).  
c   SW: ib=29 (ave.=>12) SW "bands" (CAMRT), or 31 (ave.=>14) (RRTMG);  
c   LW: ib=19 (ave.=>16) (RRTMG) (Added November 2013):  
c     ib=31  
cSOA Added December 2013  
c   SOA may be internally mixed with the SO4(ait) mode (1) or not (0).  
c   iSOA=0 in CAM4-Oslo/NorESM1 (e.g., KirkevÅg et al., 2013)  
c     iSOA=0  
cSOA
```

Let ib=31  
only for  
CAM5-Oslo  
optics and for  
the CAM4-Oslo  
AeroCom  
look-up tables  
aerodryk\*.out  
aerocomk\*.out.

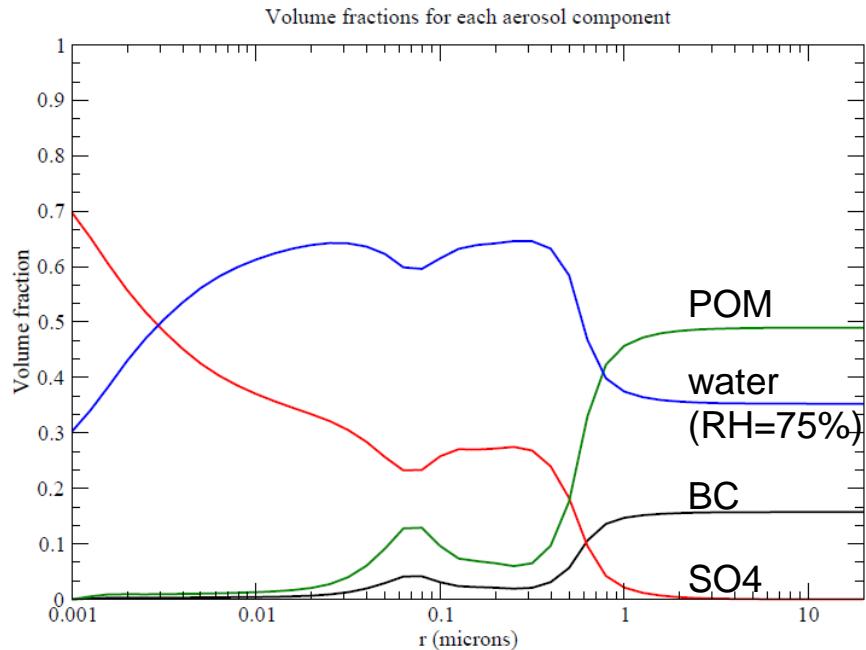
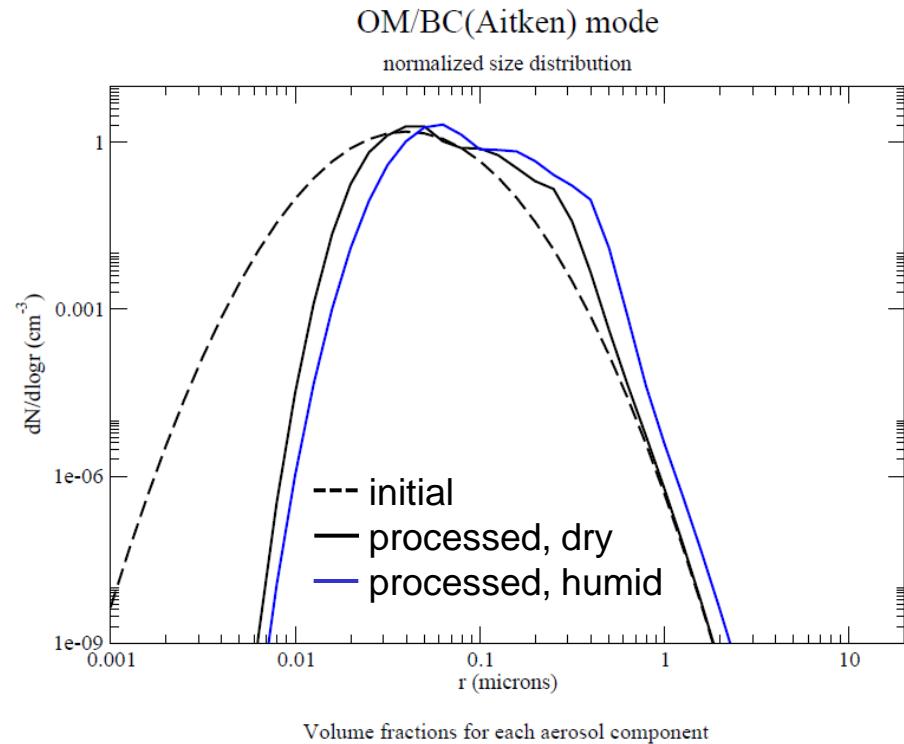
...Loop over all modes:

```
do kcomp=1,10      ! for look-up tables, kcomp=1,10 and 13 (with 13 "renamed" to 0)
```

## Aerosol growth by:

- condensation of  $\text{H}_2\text{SO}_4$
- coagulation of Aitken particles onto larger pre-existing particles
- cloud-processing/wet phase chemistry
- hygroscopic growth

$$\ln\left(\frac{e_r}{e_{s,w}}\right) = \frac{2M_w\sigma_s/r}{RT\rho_w r} - \frac{M_w}{\rho_w} \left[ \left(\frac{r}{r_0}\right)^3 - 1 \right] \sum_{\kappa} \nu_{\kappa} \Phi_{\kappa} \frac{\rho_{\kappa} \nu_{\kappa,k}(r_0)}{M_{\kappa}}$$



[20] We describe the size distribution with 44 size-bins along a logarithmic r-axis, with a bin-width of  $\Delta \log(r/\mu\text{m}) = 0.1$ . A discrete form of the continuity equation for  $N_k(r,t)$ ;

$$\frac{\partial}{\partial t} \left[ \frac{\partial N_k(r,t)}{\partial \log r} \right] + \frac{\partial}{\partial \log r} \left[ \frac{D \log r}{Dt} \frac{\partial N_k(r,t)}{\partial \log r} \right] = 0, \quad (2)$$

and similar equations for constituent mass concentrations are solved using a positive definite (anti-diffusive up-wind) advection scheme by Smolarkiewicz (1983) (*Mon. Wea. Rev.* 111, 479-486.)

[22] Following *Chuang and Penner* [1995],

$$\delta V_{aq}(r) = \frac{\Delta V_{aq}}{I_{max}} \theta(r - r_c) \left( \int \frac{dN(r)}{d \log r} \theta(r - r_c) d \log r \right)^{-1}$$

$$\delta V_{con}(r) = \frac{\Delta V_{con}}{I_{max}} r D'(r) \left( \int \frac{dN(r)}{d \log r} r D'(r) d \log r \right)^{-1}$$

and assuming coagulation of small particles onto larger size-modes:

$$\delta V_{coag}(r) = \frac{\Delta V_{coag}}{I_{max}} K_{1,2}(r, r_2) \left( \int \frac{dN(r)}{d \log r} K_{1,2}(r, r_2) d \log r \right)^{-1}$$

Hygroscopic growth of size distributions is also solved with the Smolarkiewicz scheme, but here with known growth factors,  $f(r)$  (from Köhler Eq.), instead of known process mass (e.g. condensate, from CAM-Oslo life-cycle scheme).

Continuity equations for particle number concentrations (see Kirkevåg and Iversen, 2002),

**Not a part of AeroTab,  
but related assumptions which are  
needed in CAM-Oslo, in the  
subroutine modalapp:**

(from Kirkevåg and Iversen, 2002):

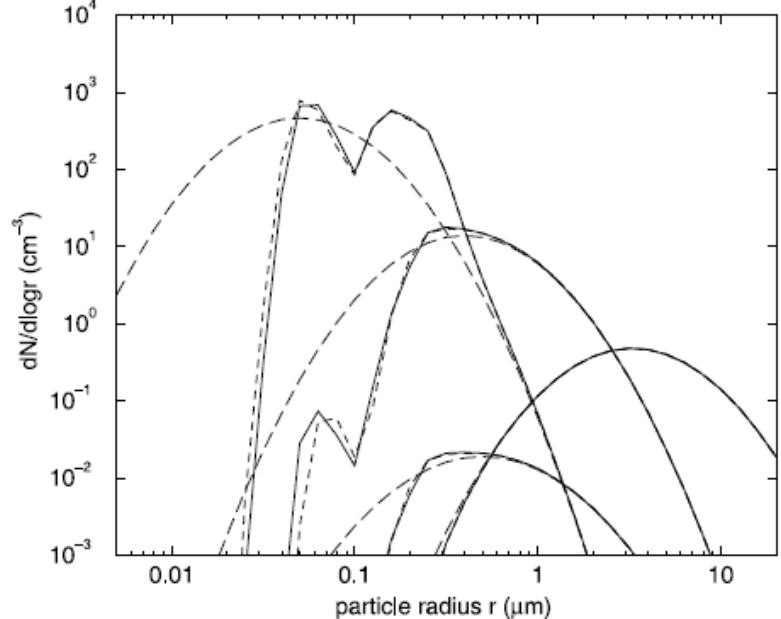
[26] Let  $\Delta V_{k,ag}$ ,  $\Delta V_{k,con}$ , and  $\Delta V_{k,coag}$  denote the integrated added volumes per volume of dry air for mode  $k$ . Integrating equations (6–8) multiplied with the total size distribution or only mode  $k$ , yields the apportionment between the modes:

$$\Delta V_{k,con} = \Delta V_{con} \left[ \int r D'(r) \frac{dN_k(r)}{d \log r} d \log r \right] \cdot \left[ \int r D'(r) \frac{dN(r)}{d \log r} d \log r \right]^{-1}, \quad (9)$$

$$\Delta V_{k,coag} = \Delta V_{coag} \left[ \int K_{1,2}(r, r_2) \frac{dN_k(r)}{d \log r} d \log r \right] \cdot \left[ \int K_{1,2}(r, r_2) \frac{dN(r)}{d \log r} d \log r \right]^{-1}, \quad (10)$$

$$\Delta V_{k,aq} = \Delta V_{aq} \left[ \int \theta(r - r_c) \frac{dN_k(r)}{d \log r} d \log r \right] \cdot \left[ \int \theta(r - r_c) \frac{dN(r)}{d \log r} d \log r \right]^{-1}. \quad (11)$$

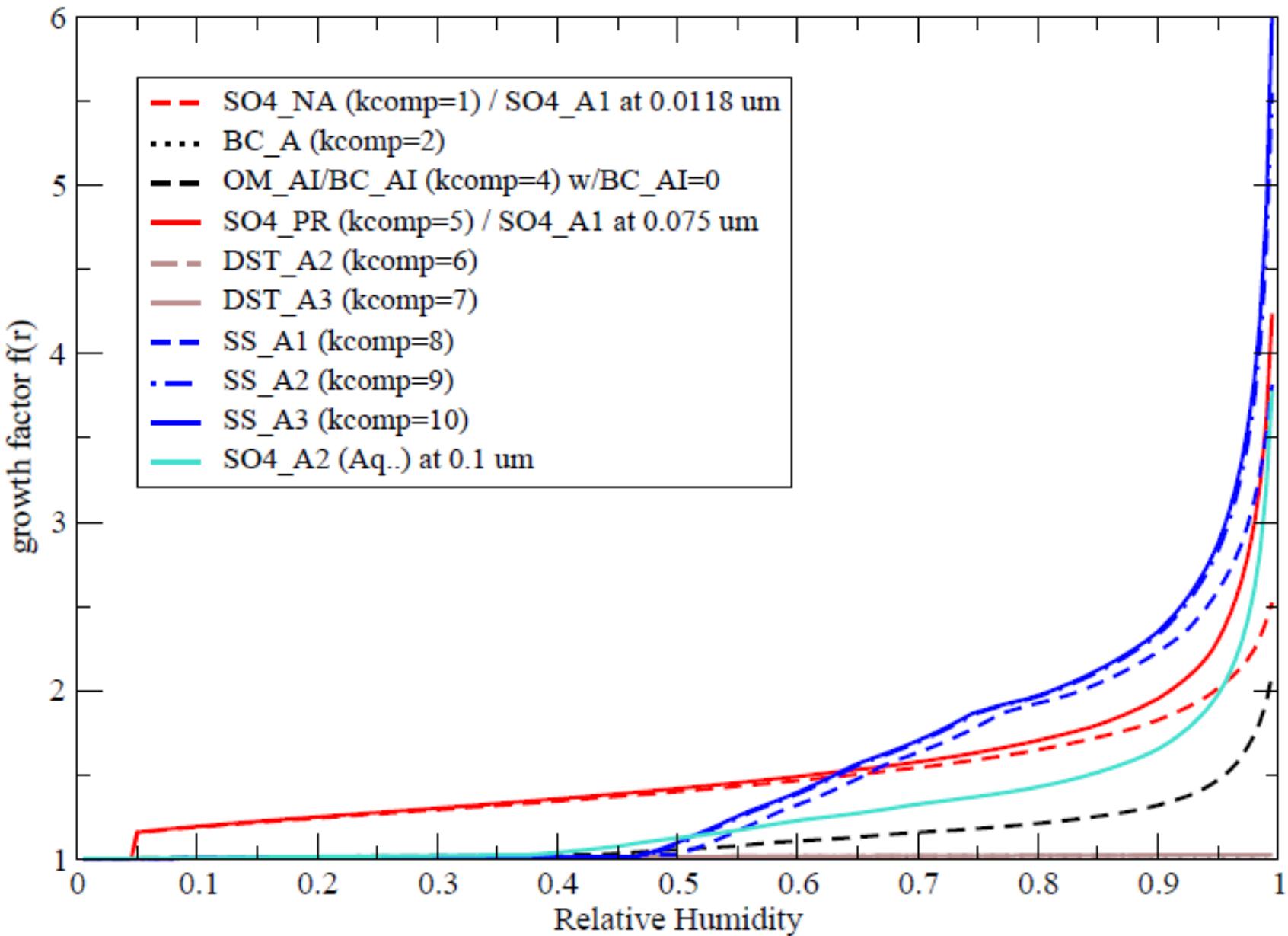
To reduce computational costs by table look-up and interpolation, we approximate equations (9–11) by using the initial size distribution in the integrands. We therefore only need to evaluate the modal apportionments for the first iteration. This approximation may displace the size-distributions, the effect of which is examined more closely in section 4, but is necessary in order to avoid solving equation (2) for the whole size distribution  $N(r)$ . Figure 1 shows an example of the effect of this approximation on a contaminated marine aerosol. The differences are negligible except for the smallest particles. For continental aerosol modes, the differences are even smaller.



**Figure 1.** Example of the effects of condensation, coagulation and cloud processing on 4 modes of a marine size distribution, where  $C^a = 10 \mu\text{g cm}^{-3}$ ,  $f_{bc} = 0.1$ , and  $f_{aq} = 0.75$ . The long-dashed curves are pure background size distributions, while the dashed and solid curves are parameterized and nonparameterized internally mixed modes.

# Hygroscopic growth

for background modes at modal radii, and internally mixed SO<sub>4</sub> at given radii



# Tracers

SO4\_N, SO4\_NA, SO4\_A1, SO4\_A2, SO4\_AC, SO4\_PR,  
 BC\_N, BC\_AX, BC\_NI, BC\_A, BC\_AI, BC\_AC  
 OM\_NI, OM\_AI, OM\_AC (OM\_N not used any more)  
 DST\_A2, DST\_A3  
 SS\_A1, SS\_A2, SS\_A3

## MIXTURES

kcomp  
CAM-  
Oslo

	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14
BC ax	SO4 na	BC a		OM ai	SO4 pr	DST a2	DST a3	SS a1	SS a2	SS a3	SO4 n	BC n	OM n	OM ni	
	SO4 a1	SO4 a1		BC ai	BC ac	BC ac	BC ac	BC ac	BC ac	BC ac				BC ni	
				SO4 a1	OM ac	OM ac	OM ac	OM ac	OM ac	OM ac					
				SO4 a2	SO4 a1	SO4 a1	SO4 a1	SO4 a1	SO4 a1	SO4 a1					
					SO4 ac	SO4 ac	SO4 ac	SO4 ac	SO4 ac	SO4 ac					
					SO4 a2	SO4 a2	SO4 a2	SO4 a2	SO4 a2	SO4 a2					

kcomp  
AeroTab 13 1 2 3 4 5 6 7 8 9 10 11, 12, 14 not used  
 (3 = OM\_A = OM\_N + condensate in older code versions) (use 1, 2, 4 with nothing added)

## Internal mixtures of process-tagged mass

**cate:** total added mass ( $\mu\text{g}/\text{m}^3$  per particle per  $\text{cm}^{-3}$ ) from condensation and wet phase chemistry/cloud processing, for  $k_{\text{comp}} = 1-2$ .

**cat:** total added mass ( $\mu\text{g}/\text{m}^3$  per particle per  $\text{cm}^{-3}$ ) from coagulation, condensation and wet phase chemistry/cloud processing, for  $k_{\text{comp}} = 5-10$ .

Cat and cate should be scaled up/down whenever the modal parameters (modal radius and width) are increased/decreased a lot.

**fac:** mass fraction of cat or cate from coagulating carbonaceous aerosols (BC+OM). The remaining mass  $\text{cate}^*(1-\text{fac})$  or  $\text{cat}^*(1-\text{fac})$  is SO<sub>4</sub>.

**fbc:** mass fraction of BC from coagulating carbonaceous aerosols, BC/(BC+OM).

**faq:** mass fraction of sulfate which is produced in wet-phase, SO<sub>4</sub><sub>aq</sub>/SO<sub>4</sub>. The remaining SO<sub>4</sub> mass, SO<sub>4</sub><sub>aq</sub><sub>\*(1-faq)</sub>, is from condensation.

**Exception**, for kcomp=4:

**Both OM and BC exist in the background size-mode** (co-emitted with same modal parameters but varying BC/OC ratio), so that only condensate or wet-phase SO<sub>4</sub> is added with varying size-dependence. To avoid making a new programming structure for this special case, we may pretend that only OM is in the background, and then add BC in a radius-independent way, before adding sulfate. New meaning of fac:

**fac:** BC mass fraction of background carbonaceous aerosols, BC/(BC+OM)

**(fbc not used:** no BC or OM coagulate on this size-mode)

**cate:** BC in the background mode + total added mass ( $\mu\text{g}/\text{m}^3$  per particle per  $\text{cm}^3$ ) from condensation and wet phase chemistry/cloud processing

```

real(r8), public, dimension(6) :: fac = (/ 0.0_r8, 0.1_r8, 0.3_r8, 0.5_r8, 0.7_r8, 0.999_r8   /)
real(r8), public, dimension(6) :: fbc = (/ 0.0_r8, 0.01_r8, 0.1_r8, 0.3_r8, 0.7_r8, 0.999_r8   /)
real(r8), public, dimension(6) :: faq = (/ 0.0_r8, 0.25_r8, 0.5_r8, 0.75_r8, 0.85_r8, 1.0_r8   /)
real(r8), public, dimension(10) :: rh = (/ 0.0_r8, 0.37_r8, 0.47_r8, 0.65_r8, 0.75_r8,
                                         &
                                         0.8_r8, 0.85_r8, 0.9_r8, 0.95_r8, 0.995_r8           /)

```

```

real(r8), public, dimension(5:10,6) :: cat = reshape ( (/ &
1.e-10_r8, 1.e-10_r8, 1.e-10_r8, 1.e-10_r8, 1.e-10_r8, 1.e-10_r8, &
5.e-4_r8 , 0.01_r8 , 0.02_r8 , 1.e-4_r8 , 0.005_r8 , 0.02_r8 , &
2.e-3_r8 , 0.05_r8 , 0.1_r8 , 6.e-4_r8 , 0.025_r8 , 0.1_r8 , &
0.01_r8 , 0.2_r8 , 0.5_r8 , 2.5e-3_r8, 0.1_r8 , 0.5_r8 , &
0.04_r8 , 0.8_r8 , 2.0_r8 , 1.e-2_r8 , 0.4_r8 , 2.0_r8 , &
0.15_r8 , 4.0_r8 , 8.0_r8 , 3.5e-2_r8, 2.0_r8 , 8.0_r8 /), (/6,6/) )

```

```

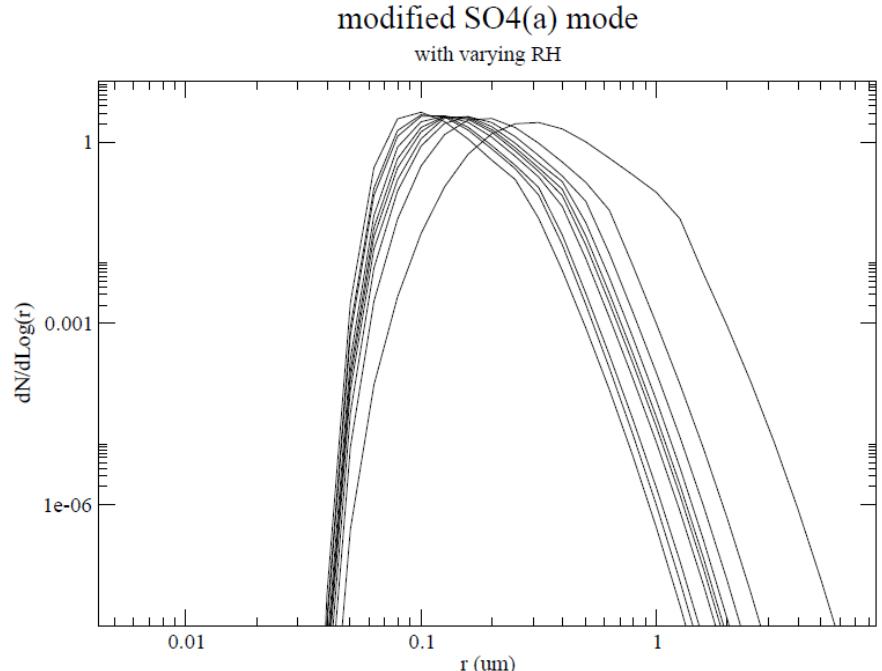
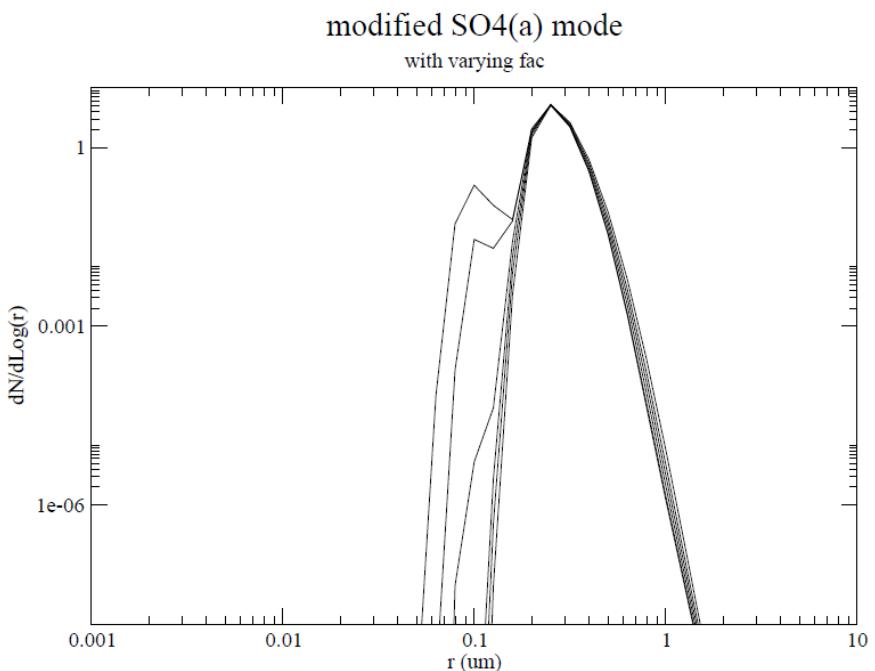
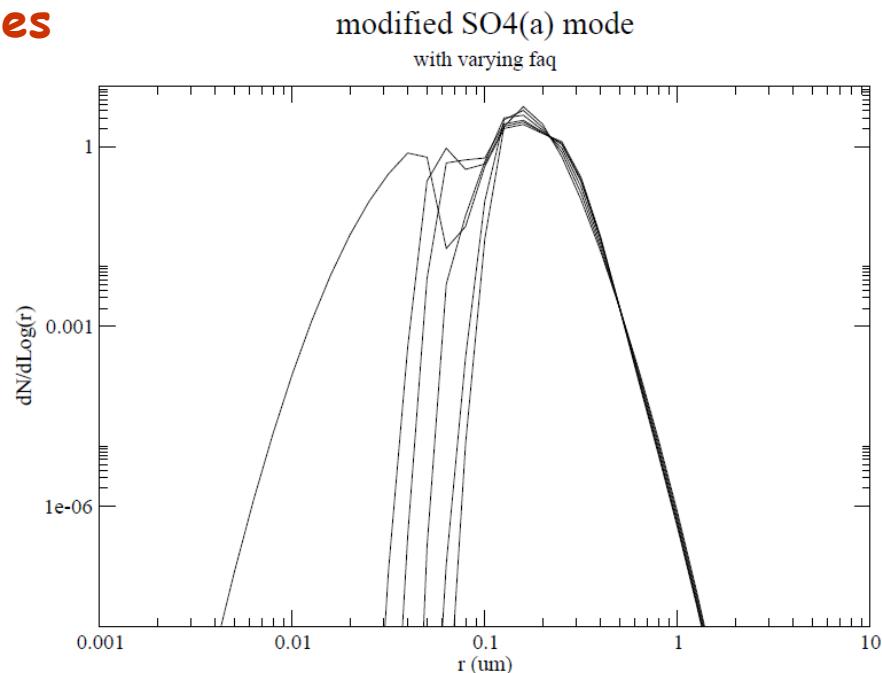
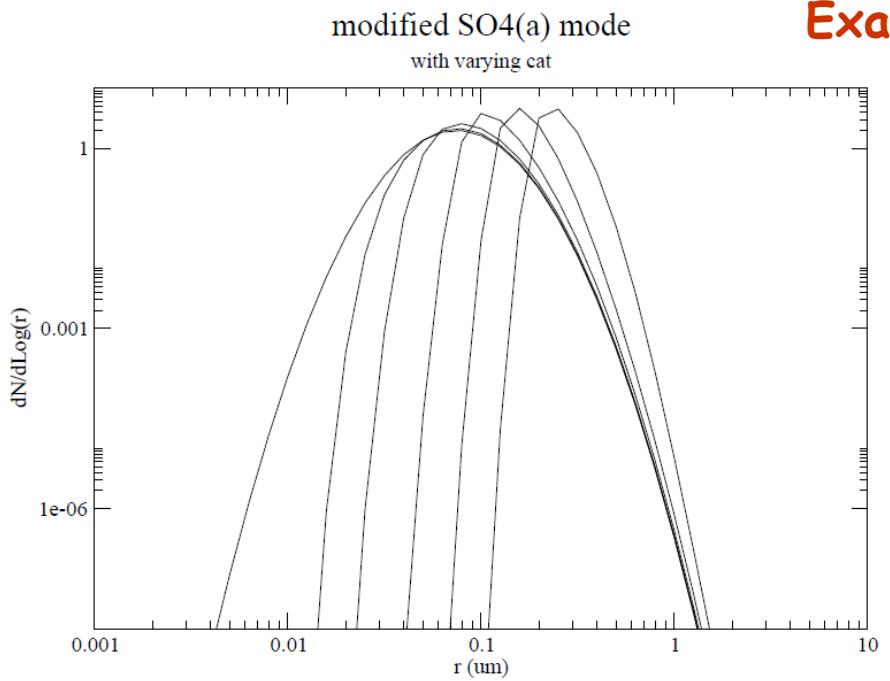
real(r8), public, dimension(4,16) :: cate = reshape ( (/ &
1.e-10_r8, 1.e-10_r8, 1.e-10_r8, 1.e-10_r8*1.904e-3_r8, &
1.e-5_r8 , 1.e-5_r8 , 1.e-4_r8 , 0.01_r8*1.904e-3_r8 , &
2.e-5_r8 , 2.e-5_r8 , 2.e-4_r8 , 0.05_r8*1.904e-3_r8 , &
4.e-5_r8 , 4.e-5_r8 , 4.e-4_r8 , 0.1_r8*1.904e-3_r8 , &
8.e-5_r8 , 8.e-5_r8 , 8.e-4_r8 , 0.2_r8*1.904e-3_r8 , &
1.5e-4_r8, 1.5e-4_r8, 1.5e-3_r8, 0.4_r8*1.904e-3_r8 , &
3.e-4_r8 , 3.e-4_r8 , 3.e-3_r8 , 0.7_r8*1.904e-3_r8 , &
6.e-4_r8 , 6.e-4_r8 , 6.e-3_r8 , 1.0_r8*1.904e-3_r8 , &
1.2e-3_r8, 1.2e-3_r8, 1.2e-2_r8, 1.5_r8*1.904e-3_r8 , &
2.5e-3_r8, 2.5e-3_r8, 2.5e-2_r8, 2.5_r8*1.904e-3_r8 , &
5.e-3_r8 , 5.e-3_r8 , 5.e-2_r8 , 5.0_r8*1.904e-3_r8 , &
1.e-2_r8 , 1.e-2_r8 , 0.1_r8 , 10.0_r8*1.904e-3_r8 , &
2.e-2_r8 , 2.e-2_r8 , 0.2_r8 , 25.0_r8*1.904e-3_r8 , &
4.e-2_r8 , 4.e-2_r8 , 0.4_r8 , 50.0_r8*1.904e-3_r8 , &
8.e-2_r8 , 8.e-2_r8 , 0.8_r8 , 100.0_r8*1.904e-3_r8 , &
0.15_r8 , 0.15_r8 , 1.5_r8 , 500.0_r8*1.904e-3_r8 /), (/4,16/) )

```

## Discrete look-up table grid values

(code from opttab.F90  
in CAM4-Oslo.  
Same as in modepar.f  
in AeroTab)

# Examples



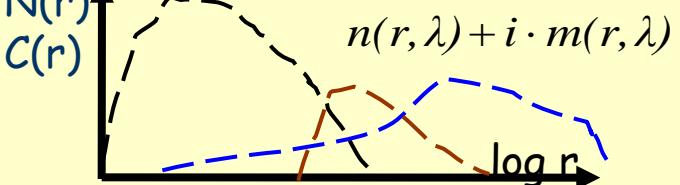
From life cycle calculations:

DU, SS and process specific  $\text{SO}_4$ , BC, OC  
+ relative humidity RH

**Principle: Scheme  
for parameterized  
optical parameters**

Cond., coag. + cloud processing  
(solve continuity eq.)

Size distribution and composition  
 $N(r)$   
 $C(r)$



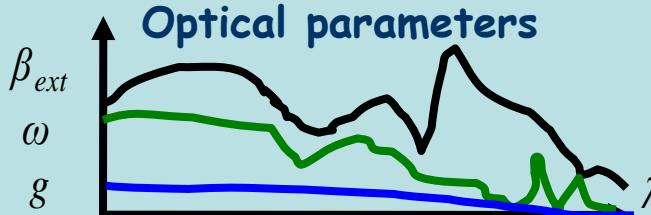
Optics  
look-up  
tables

SW:

kcomp0.out  
kcomp1.out  
...  
kcomp10.out

LW (only in  
CAM5-Oslo):  
lwkcomp0.out  
lwkcomp1.out  
...  
lwkcomp10.out

Mie theory



In CAM4/5-Oslo

Radiative  
forcing,  $\text{W/m}^2$

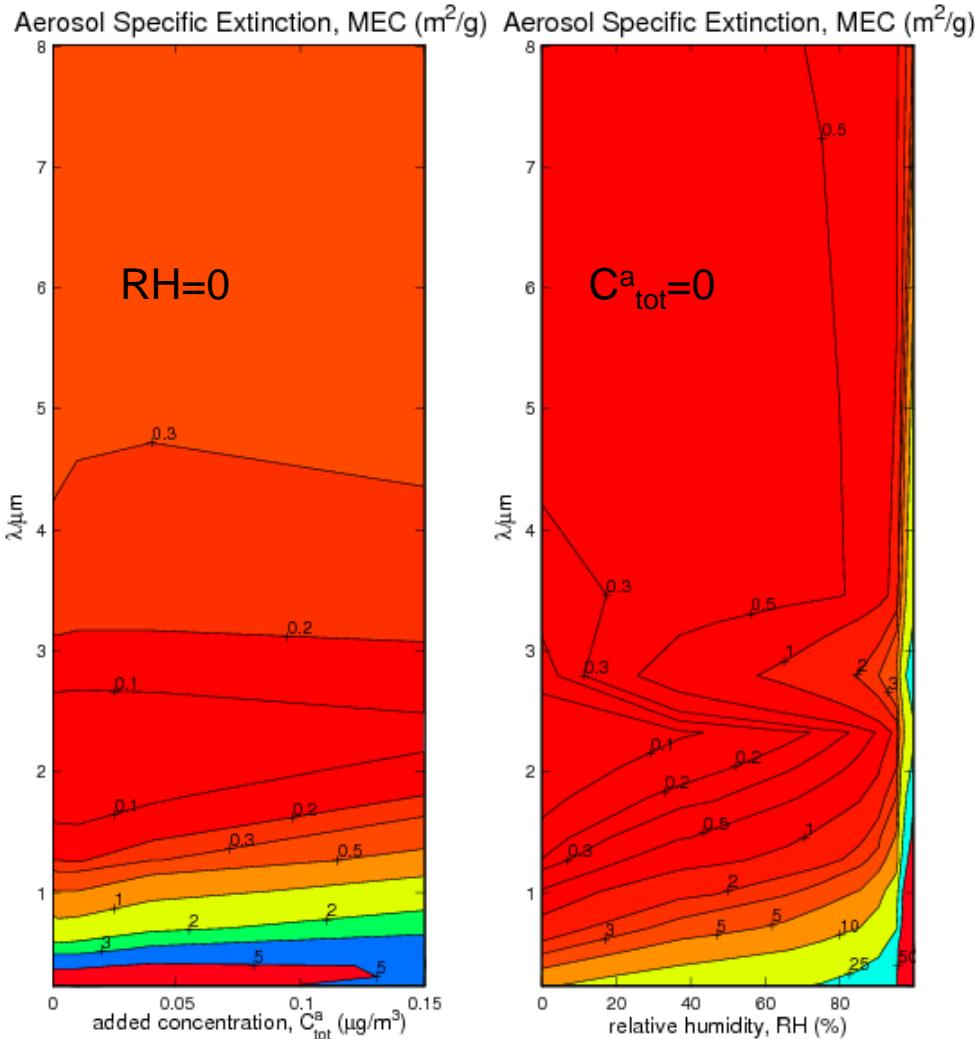
Ex. optics look-up tables for normalized size-distribution (1 cm<sup>-3</sup>):  
 SO4\_NA / SO4\_A1 mode (without SOA), kcomp1.out

<i>kcomp</i> <i>λ-band</i>	RH	catot (µg/m <sup>3</sup> )	ω (SSA)	g (ASS)	β <sub>ext</sub> (km <sup>-1</sup> )	k <sub>ext</sub> (m <sup>2</sup> /g)
1 1	0.000	0.100E-09	0.10000E+01	0.47359E+00	0.16628E-06	0.27715E+01
1 2	0.000	0.100E-09	0.10000E+01	0.39279E+00	0.71593E-07	0.11932E+01
1 3	0.000	0.100E-09	0.10000E+01	0.32032E+00	0.31281E-07	0.52137E+00
1 4	0.000	0.100E-09	0.10000E+01	0.23817E+00	0.11838E-07	0.19731E+00
1 5	0.000	0.100E-09	0.10000E+01	0.16972E+00	0.42962E-08	0.71605E-01
1 6	0.000	0.100E-09	0.99925E+00	0.10729E+00	0.13311E-08	0.22185E-01
1 7	0.000	0.100E-09	0.98957E+00	0.68222E-01	0.40892E-09	0.68156E-02
1 8	0.000	0.100E-09	0.89741E+00	0.54710E-01	0.26690E-09	0.44485E-02
1 9	0.000	0.100E-09	0.51139E+00	0.37973E-01	0.20475E-09	0.34126E-02
1 10	0.000	0.100E-09	0.17958E+00	0.28885E-01	0.29873E-09	0.49789E-02
1 11	0.000	0.100E-09	0.63999E-01	0.22469E-01	0.45194E-09	0.75325E-02
1 12	0.000	0.100E-09	0.16020E-02	0.15484E-01	0.71279E-08	0.11880E+00
1 13	0.000	0.100E-09	0.47779E-03	0.10429E-01	0.15419E-07	0.25700E+00
1 14	0.000	0.100E-09	0.23886E-04	0.17066E-02	0.26914E-07	0.44857E+00
1 1	0.000	0.100E-04	0.10000E+01	0.46974E+00	0.18902E-06	0.26923E+01
1 2	0.000	0.100E-04	0.10000E+01	0.38826E+00	0.81015E-07	0.11539E+01

(+ fac, fbc, faq for full mixtures, i.e. for kcomp5-10.out)

etc...

# Example use of output from look-up tables for SO4(a) mode using MATLAB



Mass specific extinction coefficient:

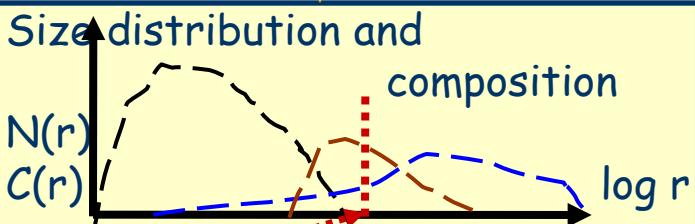
$$\text{MEC} = \beta_{\text{ext}} / C_{\text{tot}} \text{ (without water)}$$

MEC's dependence on 2 of 5 input parameters (plus  $\lambda$ ):  
total internally mixed mass, and RH

From life cycle calculations:  
DU, SS and process specific  $\text{SO}_4$ , BC, OC

**Principle:** Scheme  
for input to prognostic  
cloud droplet number  
concentrations (CDNC)

Cond., coag. + cloud processing  
(solve continuity eq.)

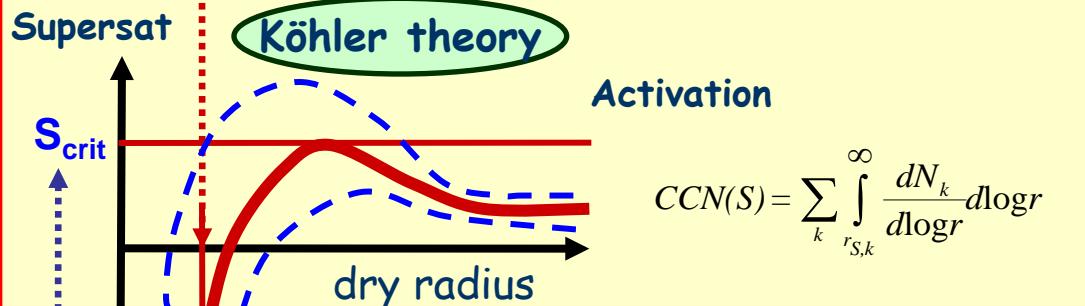


Look-up tables:  
lognormally fitted  $N(r)$

`logntilp0.out`  
`logntil1.out`

...  
`logntilp10.out`

In CAM4/5-Oslo



Activation

$$CCN(S) = \sum_k^{\infty} \int_{r_{S,k}}^{\infty} \frac{dN_k}{d\log r} d\log r$$

Calculated/realized  $S$ :  
from adiabatic lifting, assuming  
equilibrium between the  
particles and the environment  
(Abdul-Razzak and Ghan, 2000)

$CCN(S) \rightarrow$  cont.eq. for CDNC

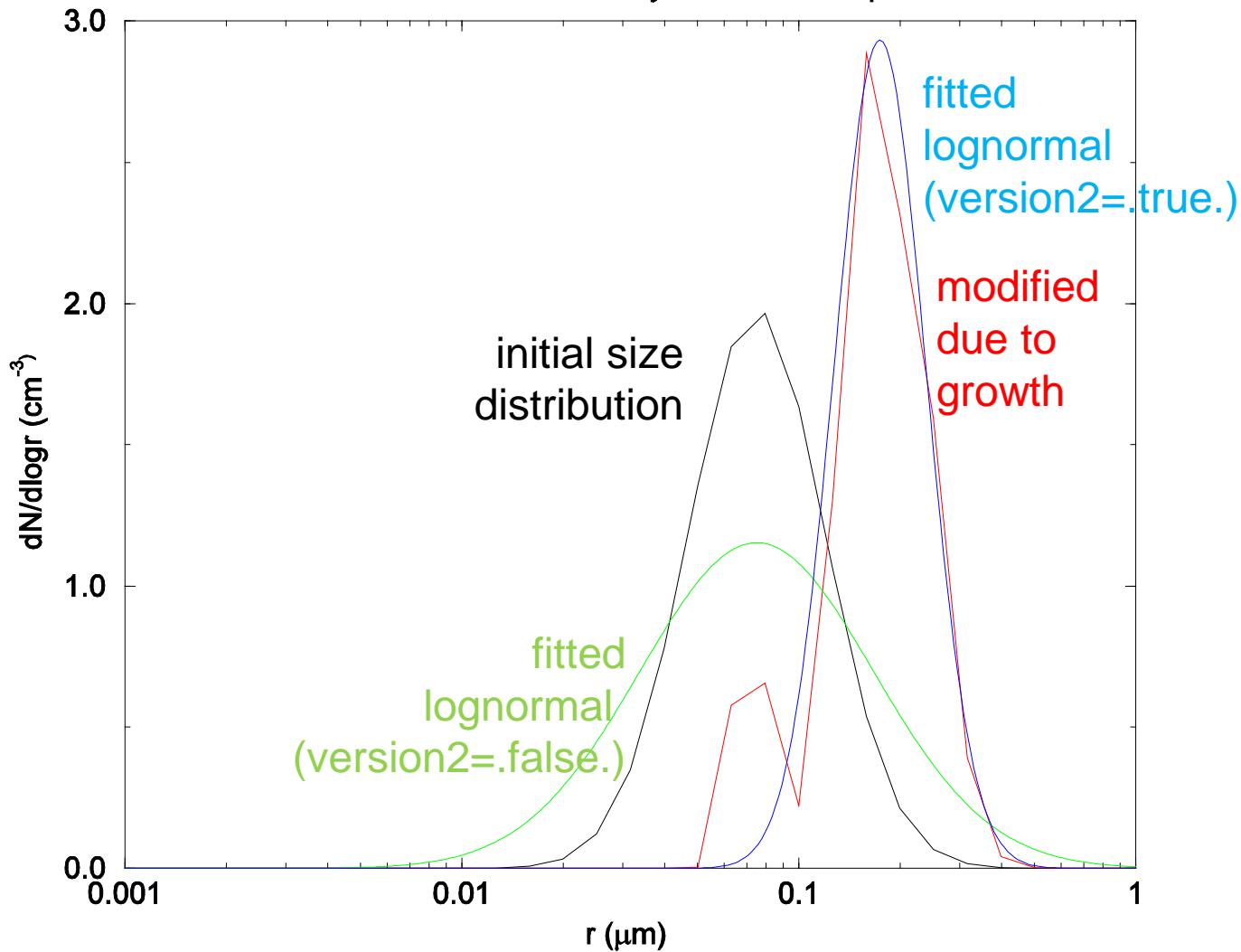
effective droplet radii,  
liquid water content

Radiative  
forcing,  $\text{W/m}^2$

Example of lognormal fitting (LUT for  $r$  and  $\sigma$ ) for use in the activation code

SO4(a)

6.6 \* increase in volume by cond. and wet phase



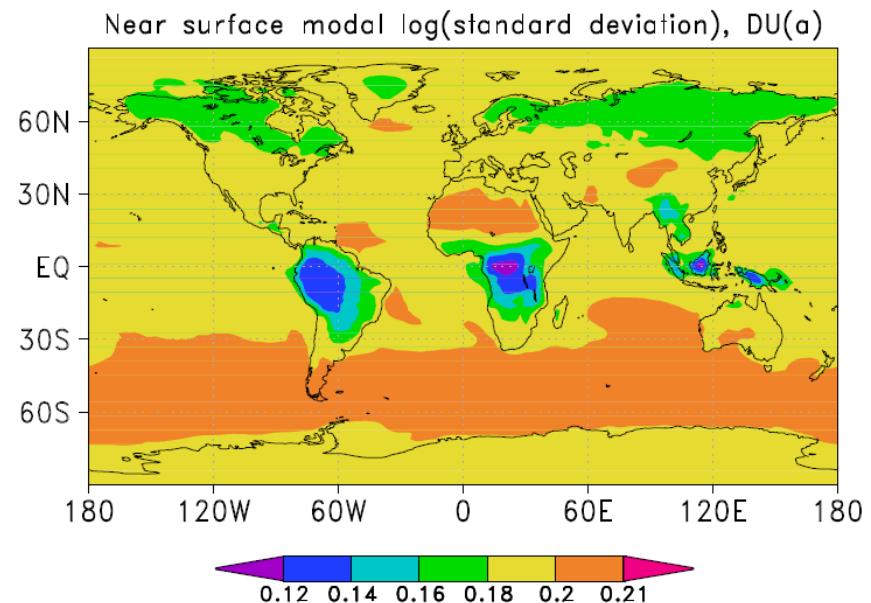
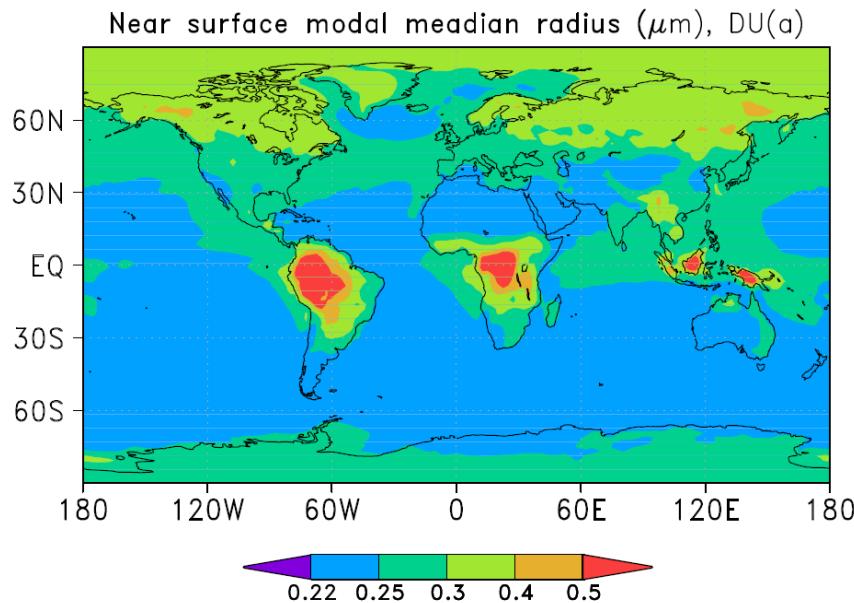
Ex. look-up tables for log-normal size parameters (dry aerosol):  
 SO4(a) mode, logntlp5.out

*kcomp*

catot ( $\mu\text{g}/\text{m}^3$ )	fac	fbc	faq	R (m)	$\log_{10}(\sigma)$	<i>kcomp</i>
0.10000E-09	0.00000E+00	0.00000E+00	0.00000E+00	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.00000E+00	0.25000E+00	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.00000E+00	0.50000E+00	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.00000E+00	0.75000E+00	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.00000E+00	0.85000E+00	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.00000E+00	0.10000E+01	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.10000E-01	0.00000E+00	0.75000E-01	0.20140E+00	5
0.10000E-09	0.00000E+00	0.10000E-01	0.25000E+00	0.75000E-01	0.20140E+00	5
etc...						
...						
0.15000E+00	0.99900E+00	0.70000E+00	0.50000E+00	0.23800E+00	0.11835E+00	5
0.15000E+00	0.99900E+00	0.70000E+00	0.75000E+00	0.23800E+00	0.11835E+00	5
0.15000E+00	0.99900E+00	0.70000E+00	0.85000E+00	0.23800E+00	0.11831E+00	5
0.15000E+00	0.99900E+00	0.70000E+00	0.10000E+01	0.23900E+00	0.11621E+00	5
0.15000E+00	0.99900E+00	0.99900E+00	0.00000E+00	0.23100E+00	0.11803E+00	5
0.15000E+00	0.99900E+00	0.99900E+00	0.25000E+00	0.23100E+00	0.11803E+00	5
0.15000E+00	0.99900E+00	0.99900E+00	0.50000E+00	0.23100E+00	0.11803E+00	5
0.15000E+00	0.99900E+00	0.99900E+00	0.75000E+00	0.23100E+00	0.11803E+00	5
0.15000E+00	0.99900E+00	0.99900E+00	0.85000E+00	0.23100E+00	0.11803E+00	5
0.15000E+00	0.99900E+00	0.99900E+00	0.10000E+01	0.23100E+00	0.11800E+00	5



## Example output from a 1 year PD simulation, CAM4-Oslo



Before growth:  $r=0.22$

(Growth here also includes hygroscopic swelling)

$\log(\sigma)=0.2014$

## **Extra output tables, e.g. for use in AeroCom**

(with #define AEROCOM in CAM-Oslo)

- |                            |  |
|----------------------------|--|
| aerodryk*.out              | Info for calculation of effective radii,<br>and dry mass concentrations for $r < 0.5 \mu\text{m}$ and $r > 1.25 \mu\text{m}$   |
| aerocomk*.out              | Species specific optical parameters for specific wavelengths<br>(440, 500, 550, 670, 870 nm, not used in standard CAM-Oslo)<br>and for $r < 0.5 \mu\text{m}$ and $r > 0.5 \mu\text{m}$ (at 550 nm). And for each<br>size-mode (kcomp), backscattering coefficient (at 550 nm). |
| and (not used in CAM-Oslo) |  |
| nkcomp*.out                | Modified aerosol number size distributions, never used   |
| ccnk*.out                  | CCN(S) for various S (no longer used)  |
- where \* = 0, 1, 2,...,10

# Extra slides

## Hygroscopic growth calculations, in koehler.f :

(... inside some do loops)

```
c      mixsub calculates hygroscopic properties (given by x)
c      for an internally mixed aerosol
$      call mixsub (frr0, itot, faq, Mw, rhow,
      j, vsk, vbck, vock, x, rh, kcomp)
c      rhumg=rhum
the Koehler equation
rhum=e**(2e3*Mw*sigm/(Rg*T*rhow*rk(i))
$      -x/((rk(i)/rk(j))**3-1.0))
```

$$\ln\left(\frac{e_r}{e_{s,w}}\right) = \frac{2M_w\sigma_{s/r}}{RT\rho_w r} - \frac{M_w}{\rho_w} \frac{1}{\left[\left(\frac{r}{r_0}\right)^3 - 1\right]} \sum_{\kappa} \nu_{\kappa} \Phi_{\kappa} \frac{\rho_{\kappa} v_{\kappa,k}(r_0)}{M_{\kappa}}$$

and calculating x in mixsub.f,  
e.g. for (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>:

```
c      ammonium sulphate:  
Ms=1.3214e2  
rhosl=1.769e3  
if(frr0.le.1.02) then  
  ai=-23.7649*frr0+24.4955  
elseif(frr0.gt.1.02.and.frr0.le.1.05) then  
  ai=10.6373*frr0-10.5947  
elseif(frr0.gt.1.05.and.frr0.le.1.11) then  
  ai=9.3474*frr0-9.2404  
elseif(frr0.gt.1.11.and.frr0.le.1.22) then  
  ai=6.2080*frr0-5.7556  
elseif(frr0.gt.1.22.and.frr0.le.1.325) then  
  ai=1.8385*frr0-0.4248  
elseif(frr0.gt.1.325.and.frr0.le.1.424) then  
  ai=-2.0065*frr0+4.6699  
elseif(frr0.gt.1.424.and.frr0.le.1.65) then  
  ai=-0.8021*frr0+2.9548  
elseif(frr0.gt.1.65.and.frr0.le.1.974) then  
  ai=-0.1192*frr0+1.8279  
elseif(frr0.gt.1.974.and.frr0.le.2.593) then  
  ai=0.1629*frr0+1.2712  
elseif(frr0.gt.2.593.and.frr0.le.3.185) then  
  ai=0.1734*frr0+1.2437  
else  
  ai=1.8  
endif  
xa=ai*(Mw/Ms)*(rhosl/rhow)
```



from offline parameterization:  
x is a function of frr0 (=r/r0)

Simplify: **x = const.**

e.g. internally mixed in mode 4, OC&BC(a):

```
elseif(kcomp.eq.4) then  
  if(itot.eq.0) then  
    x=xbg  
  else ! internal mixture  
    if(rh.lt.0.37) then  
      x=(1.0-vsk(i)-vbck(i))*xbg+vsk(i)*(1.0-faq)*xs  
    else  
      x=(1.0-vsk(i)-vbck(i))*xbg+vsk(i)*(faq*xa+(1.0-faq)*xs)  
    endif  
  endif  
23  endif!11.2014
```

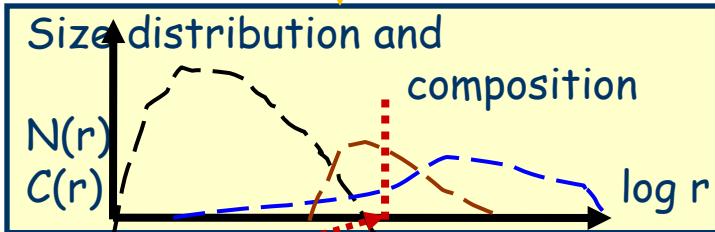
! BC or OC + H<sub>2</sub>SO<sub>4</sub> + (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>

**Principle:** Scheme for diagnostic cloud droplet number concentrations (CDNC)

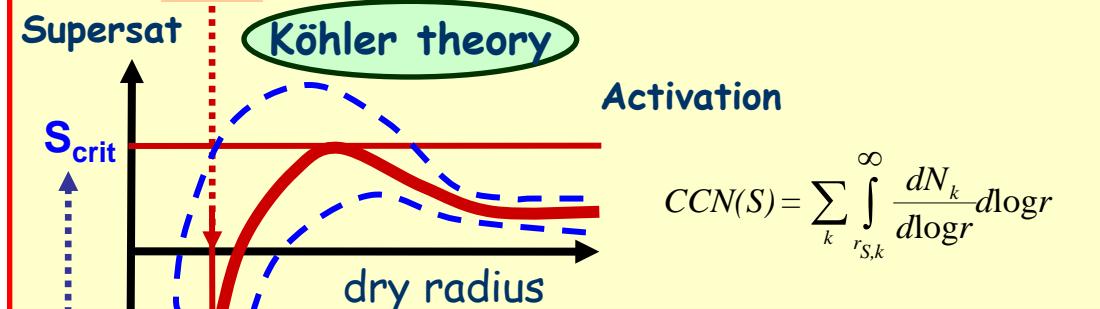
Seland et al. (2008)  
Kirkevåg et al. (2008)

From life cycle calculations:  
DU, SS and process specific  $SO_4$ , BC, OC  
+ assumed supersaturation S

Cond., coag. + cloud processing  
(solve continuity eq.)



Look-up tables



This CAM(3)-Oslo diagnostic option is not fully implemented in CAM4-Oslo !

Prescribed S:  
0.10% Stratiform clouds  
0.15% Conv. clouds over land  
0.80% Conv. clouds over ocean

$$CDNC = CCN(S)$$

effective droplet radii,  
liquid water content

Radiative forcing,  $W/m^2$